

stationary state w/ small I :

$$\text{work } \bar{W} = -f \langle \delta x \rangle$$

$$= -f^2 \sum_{n_1, n_0} W_{n_1, n_0}^{eq} p_{n_1}^{eq} c_{n_1, n_0} \delta x_{n_1, n_0}$$

$$\langle \delta x \rangle = f l \quad l \text{ some number}$$

$$\bar{W} = -f^2 l$$

$$I = -\frac{\bar{W}}{T} = \frac{f^2 l}{T} \geq 0 \Rightarrow l \geq 0 \text{ to satisfy 2nd law of therm.}$$

$$\sigma = \frac{I}{\delta t} = \text{entropy production rate}$$

$$\frac{\langle \delta x \rangle}{\delta t} \equiv J \quad \text{thermodynamic "flux"}$$

$$\frac{f}{T} \equiv \phi \quad \text{thermodynamic "force"}$$

$$\text{rewrite: } \sigma = J \phi = L \phi^2$$

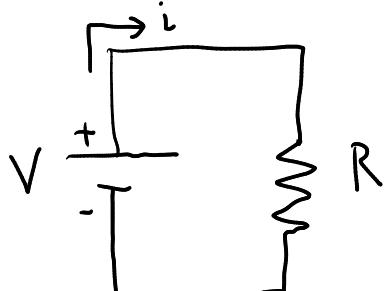
$$J = L \phi$$

Onsager
coeff.

$$L = \frac{l T}{\delta t} = \text{constant} \geq 0$$

L describes response of a sys. (th. flux) to an applied th. force ϕ

example: stationary state of an electrical circuit



power dissipated $-\frac{\bar{W}}{\delta t} = iV$

$$Q = \bar{W} = -T I$$

$$\frac{Q}{\delta t} = \frac{\bar{W}}{\delta t} = \frac{-T I}{\delta t}$$

$$-\frac{1}{T} \frac{\bar{W}}{\delta t} = \frac{I}{\delta t} = 0$$

$$i = \frac{1}{R} V$$

$$i \frac{V}{T} = 0$$

$$i = \frac{T}{R} \frac{V}{T}$$

$$\frac{T}{J} \frac{V}{\phi}$$

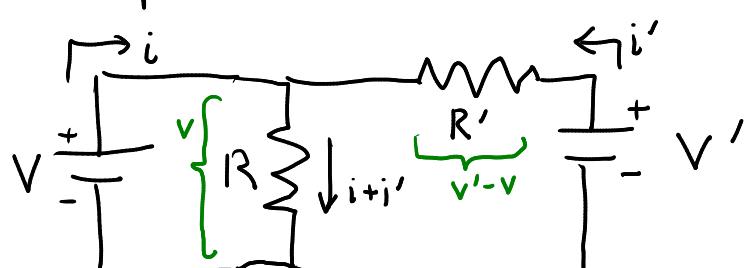
in summary:

$$T = i \quad L = \frac{T}{R} \geq 0 \Rightarrow R \geq 0$$

$$\phi = \frac{V}{T}$$

generalization: $M > 1$ therm. forces

example: $M=2$ electric circuit



total entropy prod. $\sigma = \frac{I}{T} = -\frac{1}{T} \frac{\bar{W}}{\delta t}$

$$= \frac{1}{T} [(i+i')V + i'(V'-V)]$$

$$\begin{aligned}\phi_1 &= \frac{V}{T} \\ \phi_2 &= \frac{V'}{T}\end{aligned}\quad\begin{aligned}&= i \frac{V}{T} + i' \frac{V'}{T} \\ &= J_1 \phi_1 + J_2 \phi_2\end{aligned}$$

in general: $\theta = \sum_{\alpha=1}^M J_\alpha \phi_\alpha$

$$= \vec{J} \cdot \vec{\phi}$$

J_1 = current in 1st loop
 J_2 = current in 2nd loop

$$V = (i + i')R$$

$$V' = i'R' + (i + i')R$$

$$i = \left(\frac{1}{R} + \frac{1}{R'} \right) V - \frac{1}{R'} V'$$

$$i' = -\frac{1}{R'} V + \frac{1}{R'} V'$$

$$\Rightarrow \begin{pmatrix} J_1 \\ J_2 \end{pmatrix} = \underbrace{\begin{pmatrix} \frac{1}{R} + \frac{1}{R'}, & -\frac{1}{R'} \\ -\frac{1}{R'}, & \frac{1}{R'} \end{pmatrix}}_{\text{matrix } L \text{ of Onsager coeff.}} \begin{pmatrix} \phi_1 \\ \phi_2 \end{pmatrix}$$

matrix L of Onsager coeff.

in general: $\vec{J} = L \vec{\phi}$ $L_{\alpha\gamma} = \text{transport coeff (Onsager)}$

= how much flux J_α
 we get from force ϕ_γ

$$\theta = \sum_{\alpha} J_{\alpha} \phi_{\alpha} = \sum_{\alpha\gamma} L_{\alpha\gamma} \phi_{\alpha} \phi_{\gamma}$$

$$G = \vec{\phi}^T L \vec{\phi} \geq 0 \quad \text{from 2nd law}$$

for any force $\vec{\phi}$
 (assuming linear therm.
 is valid)

What are universal properties of L ?

$\Rightarrow L$ is positive semi-definite

$$(\vec{\phi}^T L \vec{\phi} \geq 0 \quad \text{for any } \vec{\phi})$$

\Leftrightarrow eigenvals of $L \geq 0$

$\Leftrightarrow \det(L) \geq 0$

Anything else?

$$\text{Start w/ IFT: } \langle e^{-I(v)/k_B} \rangle = 1$$

$$\sum_v P(v) \underbrace{e^{-I(v)/k_B}}_{\approx 1 - \frac{I(v)}{k_B} + \frac{I^2(v)}{2k_B^2} + \dots} = 1$$

close to
equil.
all $I(v)$ small

$$1 - \frac{1}{k_B} \langle I(v) \rangle + \frac{1}{2k_B^2} \langle I^2(v) \rangle = 1$$

$$\Rightarrow \langle I(v) \rangle = \frac{1}{2k_B} \langle I^2(v) \rangle \quad [\text{Eq. 1}]$$

\Rightarrow two consequences: • Symmetry of L
 (Onsager reciprocity)

- fluctuation-dissipation theorem

focus on one-step traj: $\nu = \mu_0 = (n_0, n_1)$

$$[\text{Eq. 2}] \quad I(\nu) = k_B \ln \frac{W_{n_0, n_1} p_{n_1}^s}{W_{n_1, n_0} p_{n_0}^s}$$

$$\text{LDB: } \frac{W_{n_0, n_1}}{W_{n_1, n_0}} = e^{-\beta \left(E_{n_1} - E_{n_0} - \underbrace{\sum_{\alpha=1}^M f_\alpha \delta X_{n_0, n_1}^{(\alpha)}}_{\text{work } \omega_{n_0, n_1}} \right)}$$

$$W_{n_0, n_1}(\vec{f}) \quad p_{n_1}^s(\vec{f})$$

multiple forces

when all $f_\alpha \rightarrow 0 \Rightarrow \text{sys} \rightarrow \text{equil.}$

f_α associated w/
phys. observables

$$p_{n_1}^s = p_{n_1}^{eq} \left(1 + \sum_\alpha f_\alpha b_{n_1}^{(\alpha)} + \dots \right)$$

$$\delta X_{n_0, n_1}^{(\alpha)}$$

$$p_{n_0}^s = p_{n_0}^{eq} \left(1 + \sum_\alpha f_\alpha b_{n_0}^{(\alpha)} + \dots \right)$$

$$\frac{p_{n_1}^{eq}}{p_{n_0}^{eq}} = e^{-\beta(E_{n_1} - E_{n_0})}$$

$$p_{n_0}^{eq} = \frac{e^{-\beta E_{n_0}}}{Z}$$

$$p_{n_1}^{eq} = \frac{e^{-\beta E_{n_1}}}{Z}$$